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**UTILITY  
PATENT APPLICATION  
TRANSMITTAL**

(Only for new nonprovisional applications under 37 CFR 1.53(b))

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First Named Inventor or Application Identifier

EIGO KAWAKAMI

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**APPLICATION ELEMENTS**

See MPEP chapter 600 concerning utility patent application contents.

**ADDRESS TO:**Assistant Commissioner for Patents  
Box Patent Application  
Washington, DC 20231

1. ☐ Fee Transmittal Form  
(Submit an original, and a duplicate for fee processing)
2. ☒ Specification Total Pages
3. ☒ Drawing(s) (35 USC 113) Total Sheets
4. ☒ Oath or Declaration Total Pages
- a. ☐ Newly executed (original or copy)
- b. ☒ Unexecuted for information purposes
- c. ☐ Copy from a prior application (37 CFR 1.63(d))  
(for continuation/divisional with Box 17 completed)  
[Note Box 5 below]
- i. ☐ **DELETION OF INVENTOR(S)**  
Signed Statement attached deleting inventor(s)  
named in the prior application, see 37 CFR  
1.63(d)(2) and 1.33(b).
5. ☐ Incorporation By Reference (useable if Box 4c is checked)  
The entire disclosure of the prior application, from which a copy of the  
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6. ☐ Microfiche Computer Program (Appendix)
7. Nucleotide and/or Amino Acid Sequence Submission  
(if applicable, all necessary)
- a. ☐ Computer Readable Copy
- b. ☐ Paper Copy (identical to computer copy)
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**ACCOMPANYING APPLICATION PARTS**

8. ☐ Assignment Papers (cover sheet & document(s))
9. ☐ 37 CFR 3.73(b) Statement ☐ Power of Attorney  
(when there is an assignee)
10. ☐ English Translation Document (if applicable)
11. ☐ Information Disclosure Statement (IDS)/PTO-1449 ☐ Copies of IDS Citations
12. ☐ Preliminary Amendment
13. ☒ Return Receipt Postcard (MPEP 503)  
(Should be specifically itemized)
14. ☐ Small Entity Statement(s) ☐ Statement filed in prior application  
Status still proper and desired
15. ☐ Certified Copy of Priority Document(s)  
(if foreign priority is claimed)
16. ☐ Other: \_\_\_\_\_

17. If a CONTINUING APPLICATION, check appropriate box and supply the requisite information:

☐ Continuation ☐ Divisional ☐ Continuation-in-part (CIP) of prior application No. \_\_\_\_/\_\_\_\_**18. CORRESPONDENCE ADDRESS**☒ Customer Number or Bar Code Label05514  
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CLAIMS	(1) FOR	(2) NUMBER FILED	(3) NUMBER EXTRA	(4) RATE	(5) CALCULATIONS
	TOTAL CLAIMS (37 CFR 1.16(c))	25-20 =	5	X \$ 18.00 =	\$ 90.00
	INDEPENDENT CLAIMS (37 CFR 1.16(b))	2-3 =	0	X \$ 78.00 =	\$ 0
	MULTIPLE DEPENDENT CLAIMS (if applicable) (37 CFR 1.16(d))			\$260.00 =	\$ 0
				BASIC FEE (37 CFR 1.16(a))	\$690.00
			Total of above Calculations =		\$780.00
	Reduction by 50% for filing by small entity (Note 37 CFR 1.9, 1.27, 1.28).				
	TOTAL =				\$780.00

## 19. Small entity status

- a. ☐ A Small entity statement is enclosed
- b. ☐ A small entity statement was filed in the prior non-provisional application and such status is still proper and desired.
- c. ☐ Is no longer claimed.

20. ☒ A check in the amount of \$780.00 to cover the filing fee is enclosed.

21. ☐ A check in the amount of \$ \_\_\_\_\_ to cover the recordal fee is enclosed.

22. The Commissioner is hereby authorized to credit overpayments or charge the following fees to Deposit Account No. 06-1205:

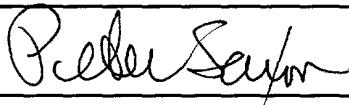
- a. ☒ Fees required under 37 CFR 1.16.
- b. ☒ Fees required under 37 CFR 1.17.
- c. ☐ Fees required under 37 CFR 1.18.

## SIGNATURE OF APPLICANT, ATTORNEY, OR AGENT REQUIRED

NAME

Peter Saxon, Esq. (Reg. No. 24,947)

SIGNATURE



DATE

May 24, 2000

PROJECTION EXPOSURE APPARATUS, AND  
DEVICE MANUFACTURING METHOD USING THE SAME

FIELD OF THE INVENTION AND RELATED ART

5           This invention relates to a projection  
exposure apparatus and a device manufacturing method  
using the same. For example, the invention is  
suitably applicable to a projection exposure apparatus  
or a scan type exposure apparatus to be used in a  
10 lithographic process, among device manufacturing  
processes for production of semiconductor devices such  
as IC or LSI, image pickup devices such as CCD,  
display devices such as a liquid crystal panel, or  
magnetic heads, for example, particularly in relation  
15 to projection of a pattern of a first object such as a  
reticle onto a second object such as a wafer through a  
projection optical system.

          As regards a microprocessing technology for  
semiconductor devices such as IC or LSI, many  
20 proposals have been made on a reduction projection  
exposure apparatus (stepper) or a scan type projection  
exposure apparatus, for forming an image of a circuit  
pattern of a mask or reticle upon a photosensitive  
substrate through a projection optical system  
25 (projection lens) and for exposing the photosensitive  
substrate in accordance with a step-and-repeat method  
or a step-and-scan method.

In these exposure apparatuses, a pattern of a reticle must be transferred onto a wafer accurately in accordance with a predetermined magnification (reduction ratio). To this end, it is important to  
5 use a projection lens (projection optical system) having a good performance and small aberrations. Particularly, in order to meet recent requirements of further miniaturization of a semiconductor device, in many cases a pattern which is beyond the normal  
10 imaging performance of a projection optical system has to be transferred to a wafer. Thus, the aberration of a projection optical system becomes very influential to the pattern to be transferred. On the other hand, for the projection lens, enlargement of an exposure  
15 area as well as enlargement of its numerical aperture (NA) are desired, which are not convenient for aberration correction.

In these circumstances, it is desired to perform measurement of the imaging performance of a  
20 projection lens, particularly, wavefront aberration thereof, in a state that the projection lens is being mounted on an exposure apparatus, that is, a state that it is used for a practical exposure process.

An example of measurement methods for  
25 wavefront aberration of a projection lens is a phase restoration method. This method has been used in the field of electron microscopes or astronomical

telescopes having large aberrations, for improvement of the resolution. In accordance with this phase restoration method, a phase distribution of an image is detected on the basis of image intensity  
5 distributions at plural positions such as image plane, pupil plane, and defocus position, for example. From the detected phase distribution, a wavefront aberration of an optical system is calculated.

In this phase restoration method, an actually  
10 measured intensity distribution of an image on an image plane is used and, after an arbitrary phase is applied, Fourier transform is made thereto to detect a complex amplitude distribution upon a pupil plane. Subsequently, while keeping a phase component of the  
15 thus detected complex amplitude distribution, only an absolute value corresponding to an intensity component thereof is replaced by a value (root square of the intensity at the pupil plane) corresponding to the actually measured value. The result is then taken as  
20 a fresh complex amplitude distribution, and inverse Fourier transform is made thereto, to determine a complex amplitude distribution upon an image plane. Again, while keeping its phase component, the intensity is replaced by an actually measured value.

25 By repeating the above-described calculations, complex amplitude distributions on the image plane and the pupil plane are calculated and,

from the phase distribution of the complex amplitude distribution at the pupil plane, the wavefront aberration of the projection lens is detected. The phase restoration method will be described later in more detail, in conjunction with preferred embodiments of the present invention.

Where a wavefront aberration of a projection lens is to be calculated in accordance with the phase restoration method, idealistically it is necessary to measure an intensity distribution of an image under a condition of coherent illumination ( $\sigma=0$ ). If the value  $\sigma$  (that is, a ratio of the numerical aperture of an illumination system to the numerical aperture of the projection lens) becomes larger, the calculated wavefront aberration contains a larger error. For example, if the wavefront aberration should be calculated with a precision of about  $0.01\lambda$ , a relation  $\sigma \leq 0.1$  is required. Even though the precision is lowered to about  $0.03\lambda$ , a relation  $\sigma \leq 0.2$  has to be satisfied. On the other hand, when a pattern of a reticle is to be photoprinted on a wafer, usually the reticle is illuminated under a partially coherent illumination condition. Thus, normally, an illumination system of an exposure apparatus has  $\sigma$  which is in a range of about  $0.2 < \sigma < 0.9$ . No illumination system as providing  $\sigma \leq 0.2$  is loaded. Further, many illumination systems for an exposure

apparatus are equipped with an incoherency-transforming mechanism.

For these reasons, when a wavefront aberration of a projection lens is to be detected in accordance with the phase restoration method while using an illumination optical system for a practical exposure process at it is, there is a problem in respect to the precision.

#### 10 SUMMARY OF THE INVENTION

It is an object of the present invention to provide a projection exposure apparatus and/or a device manufacturing method using the same, by which a wavefront aberration of a projection optical system (projection lens) for projecting a pattern of a mask onto a wafer can be measured very precisely and by which production of a large integration device can be facilitated.

These and other objects, features and advantages of the present invention will become more apparent upon a consideration of the following description of the preferred embodiments of the present invention taken in conjunction with the accompanying drawings.

25

#### BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic view of a main

portion of a projection exposure apparatus according to a first embodiment of the present invention.

Figure 2 is a schematic view of an exposure illumination system in the apparatus of Figure 1.

5           Figure 3 illustrates a first algorithm of a phase restoration method, according to the present invention.

10           Figure 4 illustrates a second algorithm of a phase restoration method, according to the present invention.

Figure 5 is a schematic view of a main portion of a projection exposure apparatus according to a second embodiment of the present invention.

15           Figure 6 is a schematic view of a main portion of a projection exposure apparatus according to a third embodiment of the present invention.

Figure 7 is a schematic view of a main portion of a projection exposure apparatus according to a fourth embodiment of the present invention.

20           Figure 8 is a schematic view of a main portion of a projection exposure apparatus according to a fifth or sixth embodiment of the present invention.

25           Figure 9 is a schematic view of a main portion of a projection exposure apparatus according to a seventh embodiment of the present invention.

Figure 10 is a schematic view of a main



portion of a projection exposure apparatus according to an eighth embodiment of the present invention.

Figure 11 is a flow chart of device manufacturing processes according to an embodiment of the present invention.

Figure 12 is a flow chart for explaining details of a wafer process, in the procedure of the flow chart of Figure 11.

## 10 DESCRIPTION OF THE PREFERRED EMBODIMENTS

Figure 1 is a schematic view of a main portion of a projection exposure apparatus according to a first embodiment of the present invention, wherein a pattern (transfer pattern) of a reticle (first object) 2 is to be projected through a projection lens 1 onto a wafer (second object) 3. As compared with a conventional exposure apparatus having a wavefront calculating mechanism based on a phase restoration method, in the apparatus of this embodiment there is a demountably mountable coherency-transforming optical system 16 being added to an exposure illumination system 13.

In the phase restoration method for detecting a wavefront aberration of the projection lens 1 in this embodiment, first, an illumination light beam IL of exposure wavelength (printing wavelength) from an exposure illumination system (illumination optical

system) 13 and passing through the incoherency-transforming optical system 16 illuminates a pattern (particular pattern) on the reticle 2 or on any other object. Then, an image of the particular pattern is  
5 formed (imaged) by the projection lens 1 upon a light intensity detecting means 8 which is mounted on a wafer stage 4. By using this intensity detecting means 8, an intensity distribution of the particular pattern image is measured. Subsequently, the wafer  
10 stage 4 is moved in an optical axis direction AX through a stage driving mechanism 5, such that, upon the light intensity detecting means 8 surface, the particular pattern image is defocused. The intensity distribution of the particular pattern image at that  
15 moment is measured. By using the results concerning the intensity distributions of these two pattern images, an information processing unit (wavefront aberration measuring means) 11 performs repeated calculations such as Fourier transform and inverse  
20 Fourier transform, for example, whereby the wavefront aberration of the projection lens 1 is calculated. It is to be noted here that the example shown in Figure 1 concerns measurement of a wavefront aberration on the optical axis of the projection optical system 1.

25           Figure 2 is a schematic view for explaining details of the exposure illumination system 13. In Figure 2, a light beam emitted from a light source 17

such as a super high pressure Hg lamp or an excimer laser, for example, is transformed into illumination light of a desired shape, by means of a light shaping unit 18 including a beam expander or a cylindrical lens, for example. The light is then projected on an incoherency-transforming unit 19.

The incoherency-transformed light from the unit 19 is then received by an illumination state adjusting unit 20 including a zoom lens, by which the illumination  $\sigma$  value is adjusted. Subsequently, the light passes a lens array (fly's eye lens optical system) 21 having its lenses arrayed two-dimensionally, and then through an exit side stop 22, whereby the effective light source is determined. After this, the light is directed to a lens system 23. Thus, with the light from the lens system 23, the reticle 2 surface can be illuminated at a desired  $\sigma$  value determined through the incoherency-transforming optical system 16.

In this embodiment, since an excimer laser is used as the light source 17, the incoherency-transforming unit 19 is provided between the light shaping unit 18 and the illumination state adjusting unit 20. If an Hg lamp, for example, for emitting incoherent light is used as the light source, use of the incoherency-transforming unit 19 is unnecessary.

When a wavefront aberration of a projection

lens 1 is to be calculated in accordance with the phase restoration method, idealistically it is necessary that the pattern of the reticle 2 is illuminated with coherent illumination ( $\sigma=0$ ). If  $0<\sigma$ ,  
5 there occurs an error in the calculation, and the error becomes larger with a larger  $\sigma$ .

On the other hand, usually a projection lens 1 of an exposure apparatus has a wavefront aberration of  $0.1\lambda$  ( $\lambda$  is the wavelength). For evaluation of such  
10 wavefront aberration, the wavefront aberration should be calculated at least at an order not greater than  $0.01\lambda$ . In order that the wavefront aberration is calculated by using the phase restoration method and with a precision not higher than  $0.01\lambda$ , the pattern of  
15 the reticle has to be illuminated with light of  $\sigma \leq 0.1$ . Further, also for qualitative evaluation of a relative change in wavefront aberration, for example, due to a change in environment caused by execution of an exposure process, a precision of an order of about  
20  $0.3\lambda$  is necessary. In that occasion, the reticle pattern should be illuminated with light of  $\sigma \leq 0.2$ .

The exposure illumination system (first illumination system) 13 is generally arranged to perform illumination of the reticle 2 in a partially  
25 coherent state or an incoherent state (first illumination condition), for practical exposure process for printing a circuit pattern on the wafer 3.

Thus, when the phase restoration method is executed only by use of the exposure illumination system 13, coherent illumination is not attainable and, therefore, the measurement has to be done while making  
5  $\sigma$  of the exposure illumination system 13 smallest. However, even a smallest value  $\sigma$  as actually loaded in a semiconductor device manufacturing exposure apparatus is about 0.3. It is therefore very difficult to calculate the wavefront aberration by the  
10 phase restoration method, with a satisfactory precision.

In this embodiment, in consideration of the above, the coherency-transforming optical system 16 is inserted between the reticle 2 and the exposure  
15 illumination system 13, for measurement of the wavefront aberration, by which the illumination light being convergent spherical wavefronts, is transformed into light of parallel wavefronts. By this, the pattern of the reticle 2 can be illuminated through  
20 coherent illumination or approximately coherent illumination (second illumination condition). As a result, high-precision wavefront aberration calculation based on the phase restoration method can be accomplished.

25 While in this embodiment the coherency-transforming optical system 16 is added to the illumination optical system 13, the coherency-

transform may be attained by removing a lens (e.g., the incoherency-transforming unit 19) of the illumination optical system 13 or by adding another optical system after the removal, for example.

5           In this embodiment as described hereinbefore, the illumination condition for the reticle is changed between an exposure process for printing a pattern of the reticle 2 on a wafer 3 and a process for calculating the wavefront aberration of the projection  
10   lens 1 based on the phase restoration method. More specifically, for the exposure process, the reticle 2 is illuminated with partially coherent light or incoherent light (first illumination condition). For the wavefront aberration calculation based on the  
15   phase restoration method, a pattern of the reticle is illuminated with coherent light or approximately coherent light ( $\sigma \leq 0.2$ , preferably,  $\sigma \leq 0.1$ ) (second illumination condition), followed by measuring light intensity distributions upon a pupil plane and a  
20   defocus plane, and detecting the wavefront aberration of the projection lens 1.

          Further, for the exposure process, the coherency-transforming optical system 16 is moved out of the light path, such that the reticle is  
25   illuminated in the partially coherent state (first illumination condition) while using the exposure illumination system 13 as it is. Then, for

measurement of the wavefront aberration based on the phase restoration method, a partial optical system is demounted from the exposure illumination system or, alternatively, the coherency-transforming optical system 16 is added thereto (of course, both may be done). By doing so, the wavefront aberration of the projection optical system can be calculated very precisely.

As an alternative, the light source may be changed so as to define best spatial coherency or best light quantity suitable for the exposure process and the phase restoration process, respectively, thereby to enable high precision calculation of the wavefront aberration of the projection optical system. As a further alternative, separate illumination optical systems (first and second optical systems) may be used for the exposure process and the phase restoration process, respectively, such that the reticle is illuminated in a partially coherent illumination state for the exposure process, while it is illuminated in a coherent or approximately coherent state for execution of measurement of the wavefront aberration of the projection lens based on the phase restoration method. This enable high precision calculation of the wavefront aberration of the projection optical system.

The second optical system may be an alignment optical system for performing alignment between a

reticle and a wafer by use of light of exposure wavelength, or it may be a portion of such alignment optical system. If the illumination condition thereof is set to  $0 \leq \sigma \leq 0.2$ , the wavefront aberration can be  
5 calculated very precisely in accordance with the phase restoration method, without addition of any optical system in the exposure apparatus, or with minimum addition of an optical system. Alternatively, the illumination condition of the alignment system may be  
10 changed between the alignment measurement process and the wavefront aberration measurement process based on the phase restoration method, to assure best measurement states, respectively.

Figures 3 and 4 illustrate algorithms based  
15 on the phase restoration method, for measurement of a wavefront aberration of a projection lens, both usable in this embodiment.

The phase restoration method method has been used in the field of electron microscopes or  
20 astronomical telescopes having large aberrations, for improvement of the resolution. In accordance with this phase restoration method, a phase distribution of an image is detected on the basis of image intensity distributions at plural positions such as image plane,  
25 pupil plane, and defocus position, for example. From the detected phase distribution, a wavefront aberration of an optical system (projection lens) is



calculated.

The algorithm of phase restoration method shown in Figure 3 will be explained first. Initially, a measured intensity distribution of an image on an image plane is used and, after an arbitrary phase is applied thereto, Fourier transform is made thereto to detect a complex amplitude distribution upon a pupil plane. Subsequently, while keeping a phase component of the thus detected complex amplitude distribution, only an absolute value corresponding to an intensity component thereof is replaced by a value (root square of the intensity at the pupil plane) corresponding to the actually measured value. The result is then taken as a fresh complex amplitude distribution, and inverse Fourier transform is made thereto, to determine a complex amplitude distribution upon an image plane. Again, while keeping its phase component, the intensity is replaced by an actually measured value. By repeating the above-described calculations, complex amplitude distributions on the image plane and the pupil plane are calculated and, from the phase distribution of the complex amplitude distribution at the pupil plane, the wavefront aberration of the lens is detected.

Figure 4 illustrates an algorithm of phase restoration method in a case where measurement of an intensity distribution upon a pupil plane is difficult

to accomplish, as in a photolithographic process. In the algorithm of Figure 4, between an image plane and a defocus plane across a pupil plane, transform and inverse transform are repeated, by which a complex amplitude distribution at the image plane and a complex amplitude distribution at the defocus plane are calculated. From the results, the phase distribution at the pupil, that is, the wavefront aberration of the projection lens is detected.

Figure 5 is a schematic view of a main portion of a projection exposure apparatus according to a second embodiment of the present invention. In Figure 5, elements corresponding to those shown in Figure 2 are denoted by like numerals.

In this embodiment, the illumination state adjusting unit 20 and the stop 22 of the exposure illumination system 13 as shown in Figure 2 are replaced by an illumination state adjusting unit 24 and a stop 25, between execution of an exposure process and execution of the phase restoration method. As shown in Figure 2, what determines the illumination condition for the exposure process is the combination of the illumination state adjusting unit 20 and the stop 22 inside the exposure illumination system 13. The illumination state adjusting unit 20 mainly comprises a zoom optical system which serves to change the size of an effective light source in accordance

with the illumination condition for the exposure process.

Generally, the value  $\sigma$  in regard to the illumination condition for wafer exposure to print a pattern on the wafer is in a range of about 0.3 to 0.8. Thus, the zoom optical system may be one covering such range. In the phase restoration method, on the other hand, a reticle must be illuminated in an approximately coherent state wherein  $\sigma$  is not greater than 0.2, preferably, not greater than 0.1. For most convenient illumination with  $\sigma$  of 0.2 or less, the aperture 22 shown in Figure 2 may be narrowed to satisfy  $\sigma \leq 0.2$ . In that occasion, since at the illumination state adjusting unit 20 the light has an expansion as of about  $\sigma=0.3$ , an eclipse may occur at the stop 22 portion and, as a result, the light quantity may decrease. Particularly, the light quantity may reduces if  $\sigma$  is not greater than 0.1. Thus, with the phase restoration method wherein the light intensity is to be measure, it may adversely influence the wavefront aberration calculation precision. While a zoom optical system that can cover a range of  $\sigma$  from 0.1 to 0.2 may be used, enlargement of the zoom ratio causes an increase in size and weight of the illumination state adjusting unit 20. Further, it becomes difficult to suppress non-uniformness of illuminance for all zoom lenses.

In this embodiment, in consideration of the above, as shown in Figure 5, for execution of the measurement of the wavefront aberration of the projection lens on the basis of the phase restoration method, the illumination state adjusting unit inside the illumination optical system 13 is replaced by the illumination state adjusting unit 24 for the phase restoration method while, on the other hand, the stop is replaced by the stop 25 to change  $\sigma$  to be not greater than 0.2. More specifically, for the exposure process, a zoom optical system with which  $\sigma$  can change from about 0.3 to about 0.8 is used in the illumination state adjusting unit 20. For execution of the phase restoration method, the illumination state adjusting unit 24 for phase restoration method which which  $\sigma$  becomes not greater than 0.2 is used. In this manner, in both of the exposure process and phase restoration process, the reticle can be illuminated with best modes, respectively. As a result of this, the wavefront of the projection lens 1 can be measured very precisely.

Figure 6 is a schematic view of a main portion of a projection exposure apparatus according to a third embodiment of the present invention. In Figure 6, elements corresponding to those of Figure 2 are denoted by like numerals.

In this embodiment, as shown in Figure 6,

fore execution of wavefront aberration measurement based on the phase restoration method, a demountable mirror 27 being movable out of the light path is inserted between a stop 22 and a lens unit 23. A  
5 second light source 26 emits light of the same wavelength as the exposure wavelength, so that, through the mirror 27 and the lens 23, a pattern on a reticle 2 is illuminated in coherent state or approximately coherent state. This differs from the  
10 first embodiment of Figure 2.

With the provision of the light source 26 for phase restoration, in addition to the exposure light source 17, the reticle 2 can be illuminated with a light quantity best suited for the phase restoration  
15 method. Thus, the wavefront aberration can be calculated very precisely. Further, while not shown in Figure 6, a lens or the like may be disposed between the second light source 26 and the mirror 27 or between the mirror 27 and the lens unit 23, for  
20 coherent illumination of the reticle.

Figure 7 is a schematic view of a main portion of a projection exposure apparatus according to a fourth embodiment of the present invention. In Figure 7, elements corresponding to those of Figure 1  
25 are denoted by like numerals. Figure 7 concerns a case wherein a wavefront aberration out of the optical axis of the projection optical system 1 is to be

detected.

In this embodiment, as shown in Figure 7, a second optical system 14 is provided, in addition to the exposure illumination system 13. For detection of a wavefront aberration of the projection lens 1 on the basis of phase restoration method, the second optical system 14 is used to illuminate a pattern on the reticle 2. Also, for an exposure process, the second optical system 14 as well as the mirror 15 move in a direction of an arrow in Figure 7 so as not interfere with the exposure light. Namely, they are demountable out of the light path. Further, the illumination condition of the second illumination optical system 14 satisfies coherent illumination ( $\sigma=0$ ) or approximately coherent illumination ( $\sigma \leq 0.2$ ). Thus, the wavefront aberration of the projection lens 1 can be measured, under an idealistic condition for the phase restoration method.

In this embodiment, it is not at all necessary to change or modify the exposure illumination system 13. Thus, an optimum illumination state for the phase restoration method is accomplished in a very simple way. The light source for the second illumination optical system 14 may comprise the same light source as the exposure light source, or it may comprise a separate light source having the same wavelength as of the exposure light source.

Figure 8 is a schematic view of a main portion of a projection exposure apparatus according to an fifth embodiment of the present invention. In Figure 8, elements corresponding to those of Figure 1 are denoted by like numerals.

In this embodiment, calculation of wavefront aberration of the projection lens 1 based on the phase restoration method can be done while using an alignment optical system for performing registration (alignment) between a reticle 2 and a wafer 3. As shown in Figure 8, the alignment optical system includes an objective lens 28, a beam splitter 29, a relay optical system 31, an illumination system relay optical system 33, a light source 34 and a sensor 30, for example. The light source 34 produces light of the same wavelength as of the exposure light, and it goes through the illumination system relay optical system 33 and the objective lens 28 to illuminate an alignment mark provided on a reticle 2. An image of the alignment mark is then formed on the sensor 30 through the objective lens 28 and the relay optical system 31. Further, through the illumination system relay optical system 33, the objective lens 28 and the projection lens 1, an alignment mark formed on the wafer 3 may be illuminated, and the mark may be imaged on the sensor 30, through the projection lens 1, the objective lens 28 and the relay optical system 33.

This enables observation of the wafer alignment mark. Alternatively, a further optical system may be disposed between the relay optical system 31 and the sensor 30, for example, if desired.

5           The phase restoration method using the above-described alignment optical system will now be explained. For the alignment measurement process, the alignment mark is illuminated usually with a condition of  $0.2 \leq \sigma \leq 1.0$ . To this end, in the alignment optical  
10 system shown in Figure 8, an interchangeable stop 32 is disposed between the illumination system relay optical system 33 and the beam splitter 29, such that the  $\sigma$  value can be changed between the alignment process and for execution of wavefront aberration  
15 measurement based on the phase restoration method. More specifically, for execution of the wavefront aberration measurement based on phase restoration, the stop is changed to provide  $\sigma \leq 0.2$ , to illuminate a pattern on the reticle. The intensity distribution of  
20 an image thereof is then measured by using a light intensity measuring system 8, by which the wavefront aberration of the projection lens 1 can be calculated. Namely, as shown in Figure 8, the interchangeable stop 32 is provided inside the alignment optical system, so  
25 that the stop is interchanged between alignment measurement and wavefront measurement based on phase restoration, thereby to assure best illumination



states for them. With this structure, without use of any additional optical system, the phase restoration method can be executed very precisely, and the wavefront aberration of the projection lens 1 can be calculated conveniently and very precisely.

While in Figure 8 the light source 34 of the alignment optical system is made separate from the exposure light source, the same light source as the exposure light source may be used. Further, the light intensity detecting system 8 in the preceding embodiments may comprise a photosensor such as a CCD which may be mounted on the stage 4. Alternatively, an enlargement optical system (not shown) may be used to enlarge the intensity distribution and, after that, it may be measured by use of the photosensor.

A sixth embodiment of the present invention will be described. The structure of this embodiment is similar to that of the fifth embodiment shown in Figure 8.

This embodiment differs from the fifth embodiment in that, on the basis of the structure that the stage 4 can be moved two-dimensionally and precisely at a nanometer order, the light intensity detecting system 8 performs measurement of a light intensity distribution upon an image plane and adjacent thereto in accordance with a knife edge method. By using the knife edge method, the light

intensity distribution can be measured very precisely without loading a heavy unit such as an enlargement optical system on the stage, as compared with a case where a photosensor is mounted directly on the stage

5 4. Alternatively, such an enlargement optical system and the knife edge method may be used in combination, to measure the light intensity distribution very precisely.

Figure 9 is a schematic view of a main  
10 portion of a projection exposure apparatus according to a seventh embodiment of the present invention. In Figure 9, elements corresponding to those of Figure 8 are denoted by like numerals.

In this embodiment, as shown in Figure 9, a  
15 reflecting portion (concave mirror portion) 9 is formed on a wafer stage 4. A pattern of a reticle 2 is imaged upon an intermediate image plane 36 by a projection lens 1. The intensity distribution of the image of the pattern is measured at the reticle 2  
20 side, and the wavefront aberration of the projection lens 1 is measured in accordance with the phase restoration method. The measurement method will be described below, in greater detail.

A second light source 34 emits light of the  
25 same wavelength as the exposure wavelength. The light goes through an illumination system relay optical system 33, an interchangeable stop 32, a beam splitter

29a and an objective lens 28, and it illuminates a pattern on the reticle 2 under an approximately coherent condition ( $\sigma$  is not greater than 0.2). While the pattern on the reticle 2 is imaged by the projection lens 1 at the same height as of the wafer 3, it is reflected by the mirror 9 formed on the wafer stage 4. Thus, the light goes again through the projection lens 1 and through a half mirror 7, it is imaged on the intermediate image plane 36. Here, the mirror 9 comprises a spherical surface mirror, and its curvature center is placed substantially at the same level as the wafer 3. The pattern of the reticle 2 being imaged on the intermediate image plane 36 after passing projection lens 1 twice, is then imaged on a sensor 30 while being magnified, through an enlargement optical system 35, a mirror 15, a beam splitter 29b, and a relay optical system 31. By moving the enlargement optical system 35 in a direction of an arrow in the drawing or by shifting the sensor 30, intensity distributions in an in-focus state and a defocus state can be measured.

With the structure described above, the measurement of the intensity distribution can be done with light passing the projection lens 1 twice. Thus, as compared with a method wherein light passes the projection lens only once, the measurement can be done with an aberration sensitivity twice higher than the

latter. Further, since the intensity distribution is imaged on the sensor 30 while being enlarged by means of the enlargement optical system 35, it can be measured with a good precision and, therefore, the wavefront aberration can be measured very precisely. Furthermore, only a mirror has to be formed on the wafer stage 4 and, conveniently, there is no necessity of mounting a heavy unit such as a sensor thereon for measurement of the light intensity distribution.

Since this embodiment is arranged like the fifth embodiment of Figure 8 so that the phase restoration method is executed by using an alignment optical system, the sensor 30, relay optical system 31, light source 34, illumination system relay optical system 33 and the objective lens 28, for example, are used in common, in both optical systems. Therefore, the phase restoration method can be executed with minimum addition of optical elements.

While in this embodiment a spherical mirror is used as the mirror 9, a flat mirror having a reflection surface placed at the same level as the wafer surface may be used. In that occasion, among the wavefront aberration components, only symmetrical components such as spherical aberration and astigmatism, for example, can be measured at a twice sensitivity. This is because light beams passing through the projection lens in the forward path (from

reticle side to wafer side) and in the backward path (from wafer side to reticle side) are revolutionally parallel to each other with respect to a principal light ray, such that asymmetrical components are cancelled. Further, while a mirror having a concave surface is shown in Figure 9, it may comprise a convex surface mirror having a curvature center placed at substantially the same level as the wafer surface.

Figure 10 is a schematic view of a main portion of a projection exposure apparatus according to an eighth embodiment of the present invention. In Figure 10, elements corresponding to those of Figure 9 are denoted by like numerals.

In this embodiment, on the basis of a wavefront aberration as calculated in accordance with the phase restoration method, an aberration correcting optical system 12 (Figure 10) disposed inside a projection lens 1 is used to perform aberration correction, or the air spacing between lens elements of the projection lens 1 is adjusted. The aberration correcting optical system 12 may comprise an optical unit having a pair of aspherical surface optical elements of the same shape, being disposed so that their aspherical surfaces are opposed to each other, as disclosed in Japanese Laid-Open Patent Application, Laid-Open No. 242048/1998.

While in Figure 10 the aberration correction

optical system 12 is disposed adjacent to a pupil plane of the projection lens 1, it may be disposed between the projection lens 1 and the wafer 3 or between the projection lens 1 and the reticle 2.

5 Alternatively, plural elements may be disposed there.

In the embodiments described above, the wavefront aberration of the projection lens 1 is calculated on the basis of a focus plane (image plane) and one defocus plane. However, it can be calculated  
10 from intensity distributions of images at two different defocus planes, without using the focus plane (image plane). Further, the wavefront aberration can be calculated by using intensity distributions of images at three or more positions  
15 including a focus plane (image plane) and plural defocus planes. Furthermore, while an example of aberration correcting optical system comprising a pair of aspherical surface optical elements has been described, the invention is not limited to it. The  
20 aberration correction may be accomplished by moving plural lenses in a projection lens system, or by disposing one or more parallel flat plates between the projection lens and the wafer or between the projection lens and the reticle and by changing the  
25 angles of these parallel flat plates.

A projection exposure apparatus according to any one of the preceding embodiments may be used so

that, after detection of the relative position between  
a mask and a wafer, a pattern on the mask surface is  
transferred to the wafer surface. Thereafter, the  
wafer is processed by a development treatment, for  
5 production of devices.

Between such exposure process and execution  
of phase restoration method, the illumination  
condition can be changed, such that, within the major  
assembly of the exposure apparatus, a wavefront  
10 aberration of the projection lens can be calculated  
very precisely in accordance with the phase  
restoration method. Particularly, for execution of  
the phase restoration method, an optical system may be  
added to the exposure illumination system or only a  
15 portion of the exposure illumination system is used so  
as to assure that a reticle is illuminated in an  
approximately coherent condition. Alternatively, the  
illumination optical system may be changed by  
replacing a portion thereof, for example. In this  
20 manner, the wavefront aberration can be measured very  
precisely.

For execution of phase restoration method, as  
described above, a second optical system different  
from the exposure illumination system may be used to  
25 illuminate a reticle in an approximately coherent  
state. The wavefront aberration of the projection  
lens can be calculated very precisely, also in such

case, in accordance with the phase restoration method and inside the major assembly of the exposure apparatus. The second optical system may comprise an alignment optical system. Thus, without any  
5 additional optical system, the wavefront aberration of the projection lens can be calculated very precisely in accordance with the phase restoration method and inside the major assembly of the exposure apparatus.

In accordance with the thus calculated  
10 wavefront aberration, an aberration correcting optical system, for example, disposed outside the projection lens, may be used to adjust the wavefront aberration of the projection lens. This enables an exposure process with small wavefront aberration.

15 While the foregoing embodiments have been described with reference to a step-and-repeat type projection exposure apparatus for manufacture of semiconductor devices, the invention is applicable also to a scanning exposure apparatus or an exposure  
20 apparatus for liquid crystal devices.

Next, an embodiment of a semiconductor device manufacturing method which uses a projection exposure apparatus according to any one of the preceding embodiments, will be explained.

25 Figure 10 is a flow chart of procedure for manufacture of microdevices such as semiconductor chips (e.g. ICs or LSIs), liquid crystal panels, CCDs,



thin film magnetic heads or micro-machines, for example.

Step 1 is a design process for designing a circuit of a semiconductor device. Step 2 is a process for making a mask on the basis of the circuit pattern design. Step 3 is a process for preparing a wafer by using a material such as silicon. Step 4 is a wafer process (called a pre-process) wherein, by using the so prepared mask and wafer, circuits are practically formed on the wafer through lithography. Step 5 subsequent to this is an assembling step (called a post-process) wherein the wafer having been processed by step 4 is formed into semiconductor chips. This step includes an assembling (dicing and bonding) process and a packaging (chip sealing) process. Step 6 is an inspection step wherein operation check, durability check and so on for the semiconductor devices provided by step 5, are carried out. With these processes, semiconductor devices are completed and they are shipped (step 7).

Figure 11 is a flow chart showing details of the wafer process.

Step 11 is an oxidation process for oxidizing the surface of a wafer. Step 12 is a CVD process for forming an insulating film on the wafer surface. Step 13 is an electrode forming process for forming electrodes upon the wafer by vapor deposition. Step

14 is an ion implanting process for implanting ions to the wafer. Step 15 is a resist process for applying a resist (photosensitive material) to the wafer. Step 16 is an exposure process for printing, by exposure, the circuit pattern of the mask on the wafer through the exposure apparatus described above. Step 17 is a developing process for developing the exposed wafer. Step 18 is an etching process for removing portions other than the developed resist image. Step 19 is a resist separation process for separating the resist material remaining on the wafer after being subjected to the etching process. By repeating these processes, circuit patterns are superposedly formed on the wafer.

With these processes, high density microdevices can be manufactured.

In accordance with the embodiments described hereinbefore, a wavefront aberration of a projection optical system (projection lens) for projecting a mask pattern onto a wafer can be measured very precisely. Thus, with the present invention, a projection exposure apparatus or a device manufacturing method which facilitates production of large integration devices is accomplished.

While the invention has been described with reference to the structures disclosed herein, it is not confined to the details set forth and this application is intended to cover such modifications or

changes as may come within the purposes of the  
improvements or the scope of the following claims.

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WHAT IS CLAIMED IS:

1. A projection exposure apparatus, comprising:
  - a projection optical system for projecting a transfer pattern of a first object onto a second
  - 5 object;
  - a first illumination system for performing illumination under a first illumination condition, wherein the transfer pattern of the first object illuminated under the first illumination condition is
  - 10 projected onto the second object through said projection optical system;
  - a second illumination system for performing illumination under a second illumination condition;
  - a light intensity detector; and
  - 15 an information processing system operable, as a particular pattern being illuminated by said second illumination system under the second illumination condition is imaged by said projection optical system, to measure a wavefront aberration of said projection
  - 20 optical system on the basis of detection of a light intensity distribution of an image of the particular pattern made through said light intensity detector.
2. An apparatus according to Claim 1, wherein
- 25 said information processing system is arranged to detect a phase distribution of the image of the particular pattern on the basis of light intensity

distributions defined in relation to that image at  
different positions along an optical axis direction of  
said projection optical system, and to measure the  
wavefront aberration of said projection optical system  
5 on the basis of the detected phase distribution.

3. An apparatus according to Claim 1, wherein  
the second object is a photosensitive substrate, and  
wherein said projection optical system is used to  
10 project and print the transfer pattern, being  
illuminated under the first illumination condition,  
onto an exposure region on the photosensitive  
substrate.

15 4. An apparatus according to Claim 1, wherein  
said information processing system is arranged to  
measure the wavefront aberration of said projection  
optical system on the basis of light intensity  
distributions detected with respect to an imaging  
20 position of the image of the particular pattern and at  
least one defocus position of thereof, or of light  
intensity distributions with respect to different  
positions.

25 5. An apparatus according to Claim 4, wherein  
said information processing system measures the  
wavefront aberration of said projection optical system

in accordance with a phase restoration method.

6. An apparatus according to Claim 4, wherein  
said first and second illumination systems include a  
5 common element.

7. An apparatus according to Claim 1, wherein  
said first and second illumination systems are  
different in respect to a spatial coherency.  
10

8. An apparatus according to Claim 7, wherein  
the first illumination condition concerns being  
spatially partially coherent or being incoherent, and  
wherein said second illumination condition concerns  
15 being spatially coherent or being approximately  
coherent.

9. An apparatus according to Claim 7, wherein,  
in each of said first and second illumination systems,  
20 a ratio of a numerical aperture of said first or  
second illumination system to a numerical aperture of  
said projection optical system is  $\sigma$ , and wherein the  
first illumination condition satisfies a relation  
 $0.2 < \sigma \leq 1.0$  while the second illumination condition  
25 satisfies a relation  $\sigma \leq 0.2$ .

10. An apparatus according to Claim 7, wherein

said first and second illumination systems include a common element.

11. An apparatus according to Claim 10, further  
5 comprising a separate optical system which can be demountably added to said common element, to thereby interchange the first and second illumination conditions each other.

10 12. An apparatus according to Claim 10, wherein interchanging the first and second illumination conditions each other is performed by changing a light source to said common element.

15 13. An apparatus according to Claim 1, wherein said first and second illumination systems use different optical systems.

14. An apparatus according to Claim 13, wherein  
20 the optical system of said second illumination system has an additional use, other than for detection of wavefront aberration information.

15. An apparatus according to Claim 14, wherein  
25 said second illumination optical system is arranged to change its illumination condition between for the detection of wavefront aberration information and for

the additional use.

16. An apparatus according to Claim 15, wherein,  
for the detection of the wavefront aberration  
5 information, said second illumination system sets an  
illumination condition satisfying a relation  $\sigma \leq 0.2$   
where  $\sigma$  is a ratio of a numerical aperture of said  
second illumination system to a numerical aperture of  
said projection optical system.

10

17. An apparatus according to Claim 15, wherein,  
for the detection of the wavefront aberration  
information, said second illumination system sets an  
illumination condition satisfying a relation  $\sigma = 0$  where  
15  $\sigma$  is a ratio of a numerical aperture of said second  
illumination system to a numerical aperture of said  
projection optical system.

18. An apparatus according to Claim 13, wherein  
20 said first and second illumination systems use  
different light sources.

19. An apparatus according to Claim 1, wherein  
said light intensity detector measures a light  
25 intensity distribution in accordance with a knife edge  
method.



20. An apparatus according to Claim 1, further comprising an enlarging optical system for enlarging a light intensity distribution to be incident on said light intensity detector.

5

21. An apparatus according to Claim 1, further comprising an adjusting mechanism for adjusting an aberration of said projection optical system on the basis of wavefront aberration information detected by  
10 said information processing system.

22. An apparatus according to Claim 1, further comprising means for adjusting an aberration of said projection optical system, prior to projection of the  
15 transfer pattern onto the second object through said projection optical system, on the basis of wavefront aberration information detected by said information processing system and information related to the transfer pattern.

20

23. An apparatus according to Claim 1, wherein said second illumination system is usable for alignment between the first and second objects.

25

24. A device manufacturing method, comprising:  
a projection exposure step for projecting a pattern of a reticle onto a wafer by use of a

projection exposure apparatus including (i) a  
projection optical system for projecting a transfer  
pattern of the reticle onto the wafer, (ii) a first  
illumination system for performing illumination under  
5 a first illumination condition, wherein the transfer  
pattern of the reticle illuminated under the first  
illumination condition is projected onto the wafer  
through the projection optical system, (iii) a second  
illumination system for performing illumination under  
10 a second illumination condition, (iv) a light  
intensity detector, and (v) an information processing  
system operable, as a particular pattern being  
illuminated by the second illumination system under  
the second illumination condition is imaged by the  
15 projection optical system, to measure a wavefront  
aberration of the projection optical system on the  
basis of detection of a light intensity distribution  
of an image of the particular pattern made through the  
light intensity detector; and

20 a developing step for developing the wafer  
processed by said projection exposure step, whereby  
a device can be produced from the developed wafer.

25 25. A method according to Claim 24, further  
comprising an adjusting step for adjusting an  
aberration of the projection optical system on the  
basis of the detected wavefront aberration.

ABSTRACT OF THE DISCLOSURE

A projection exposure apparatus includes a projection optical system for projecting a transfer pattern of a first object onto a second object, a  
5 first illumination system for performing illumination under a first illumination condition, wherein the transfer pattern of the first object illuminated under the first illumination condition is projected onto the second object through the projection optical system, a  
10 second illumination system for performing illumination under a second illumination condition, a light intensity detector, and an information processing system operable, as a particular pattern being illuminated by the second illumination system under  
15 the second illumination condition is imaged by the projection optical system, to measure a wavefront aberration of the projection optical system on the basis of detection of a light intensity distribution of an image of the particular pattern made through the  
20 light intensity detector.

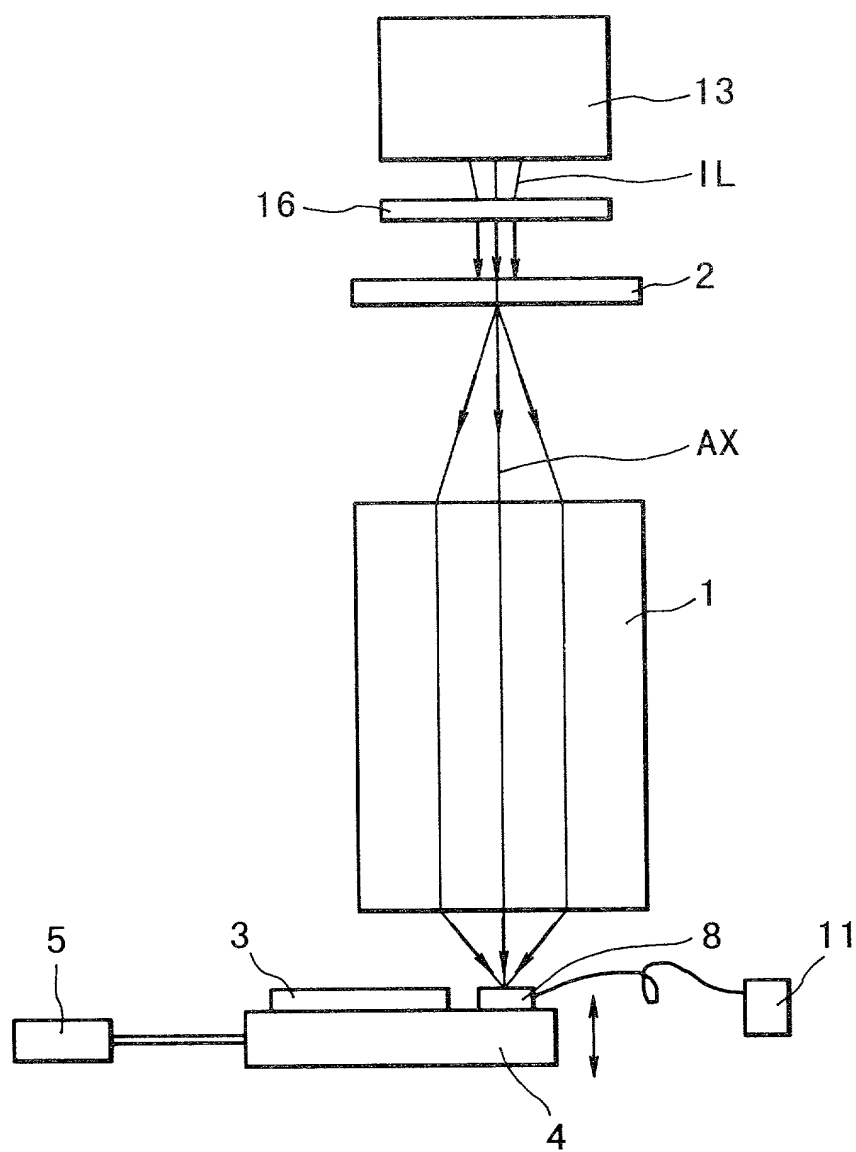
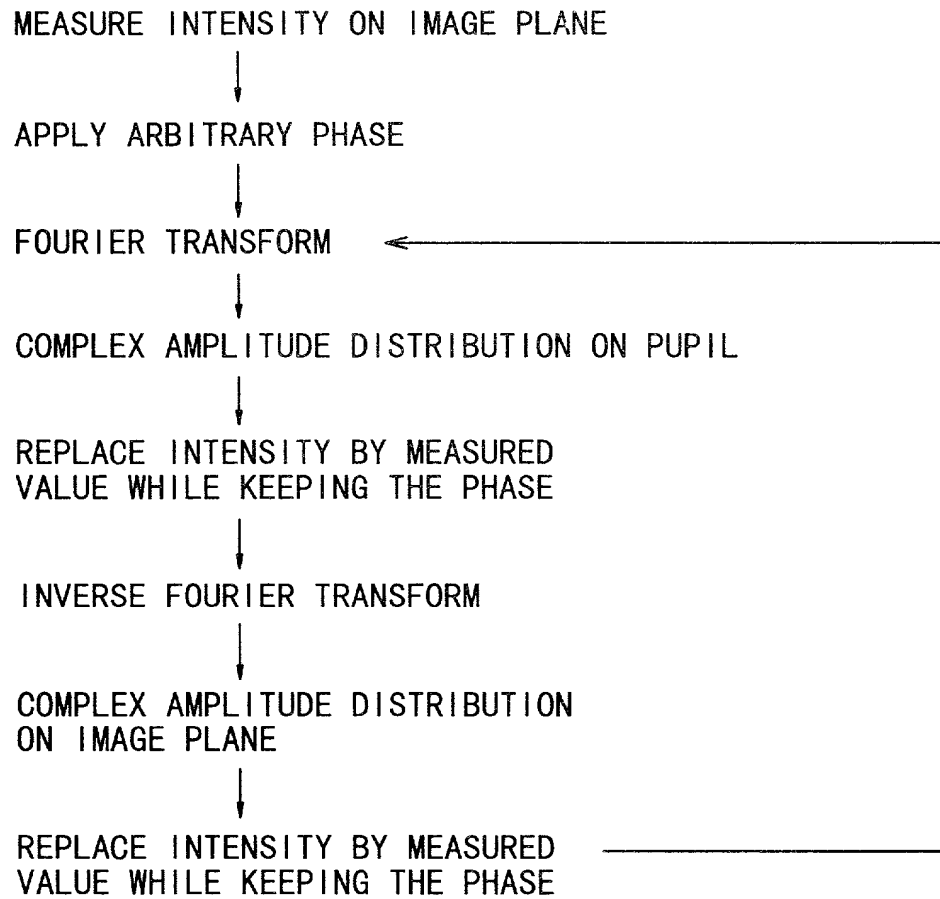
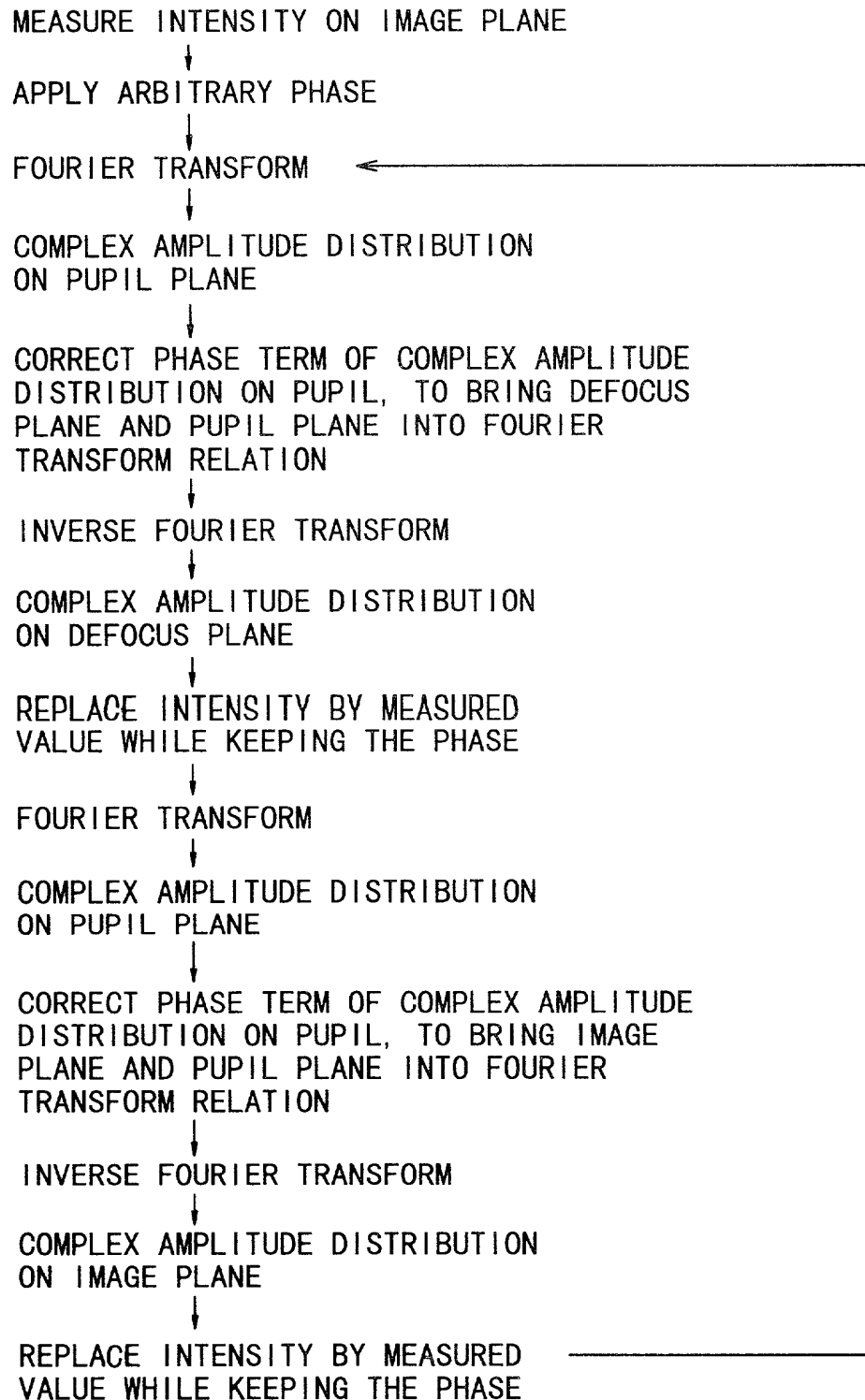


FIG. 1





**FIG. 3**



**FIG. 4**

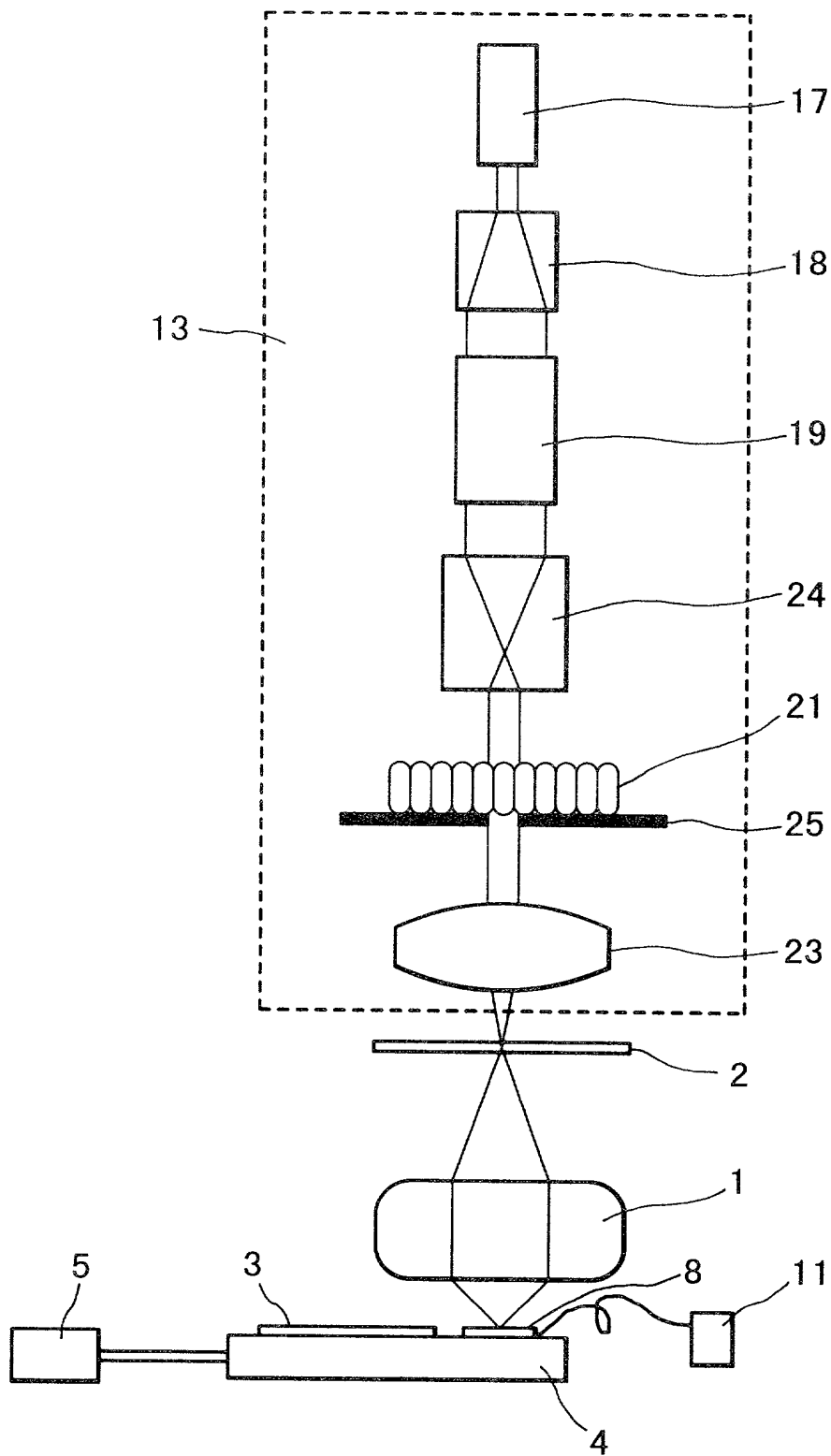
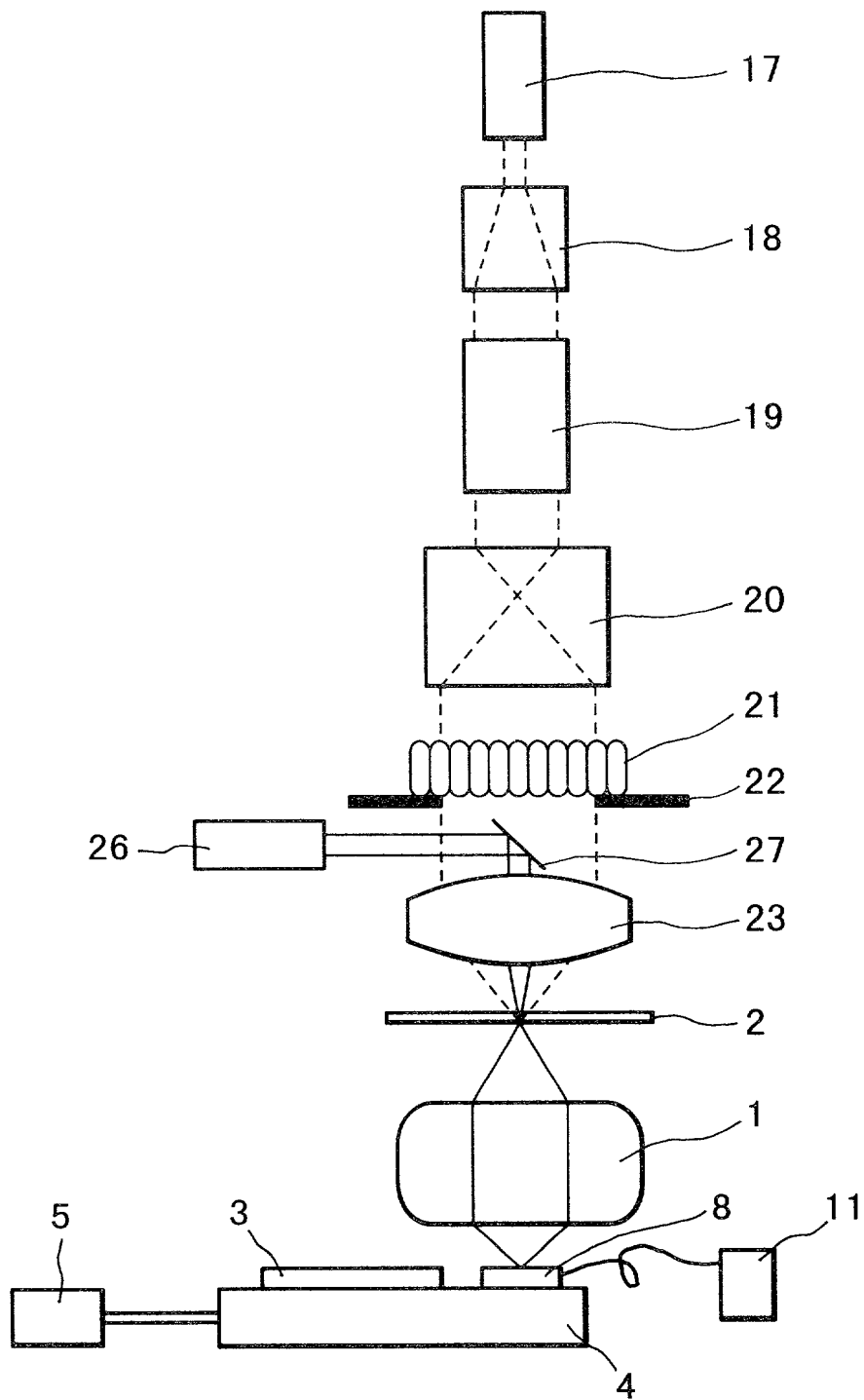


FIG. 5





**FIG. 6**

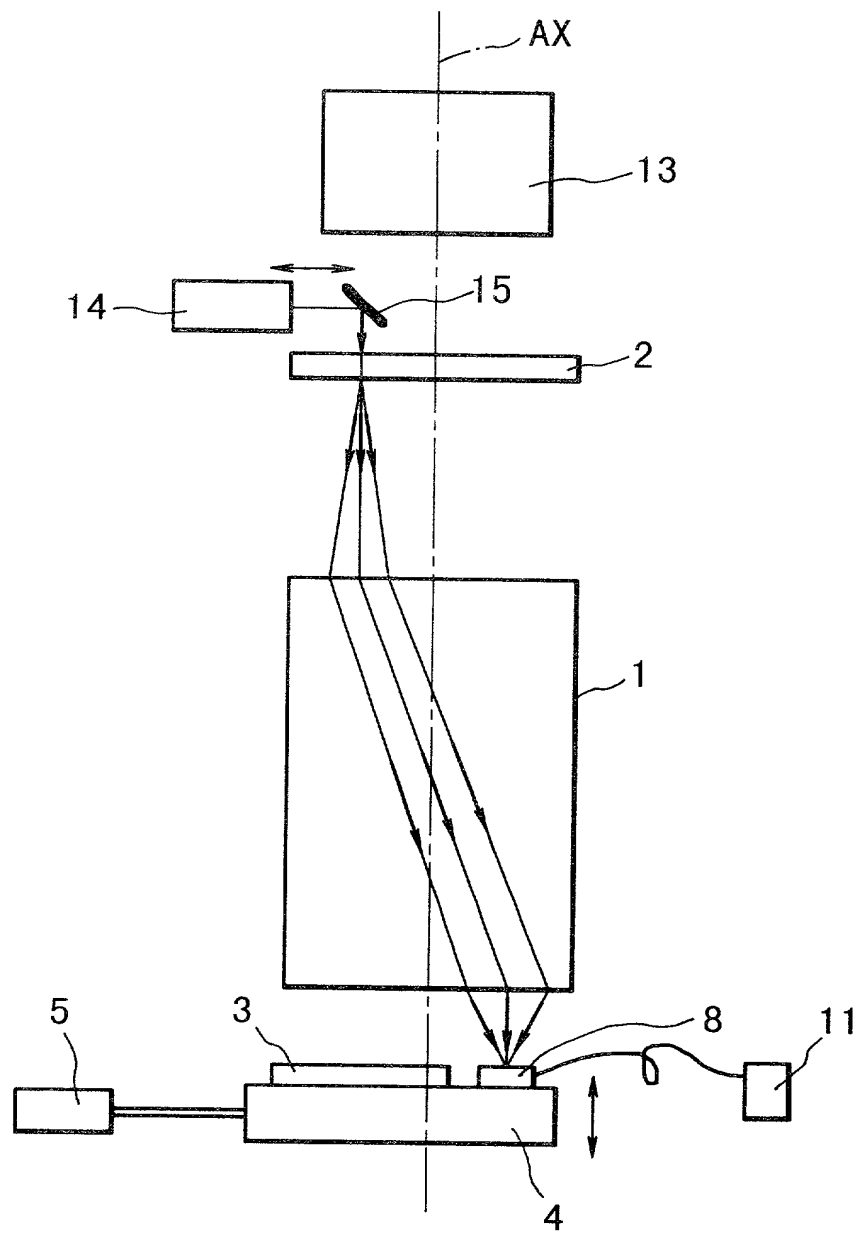
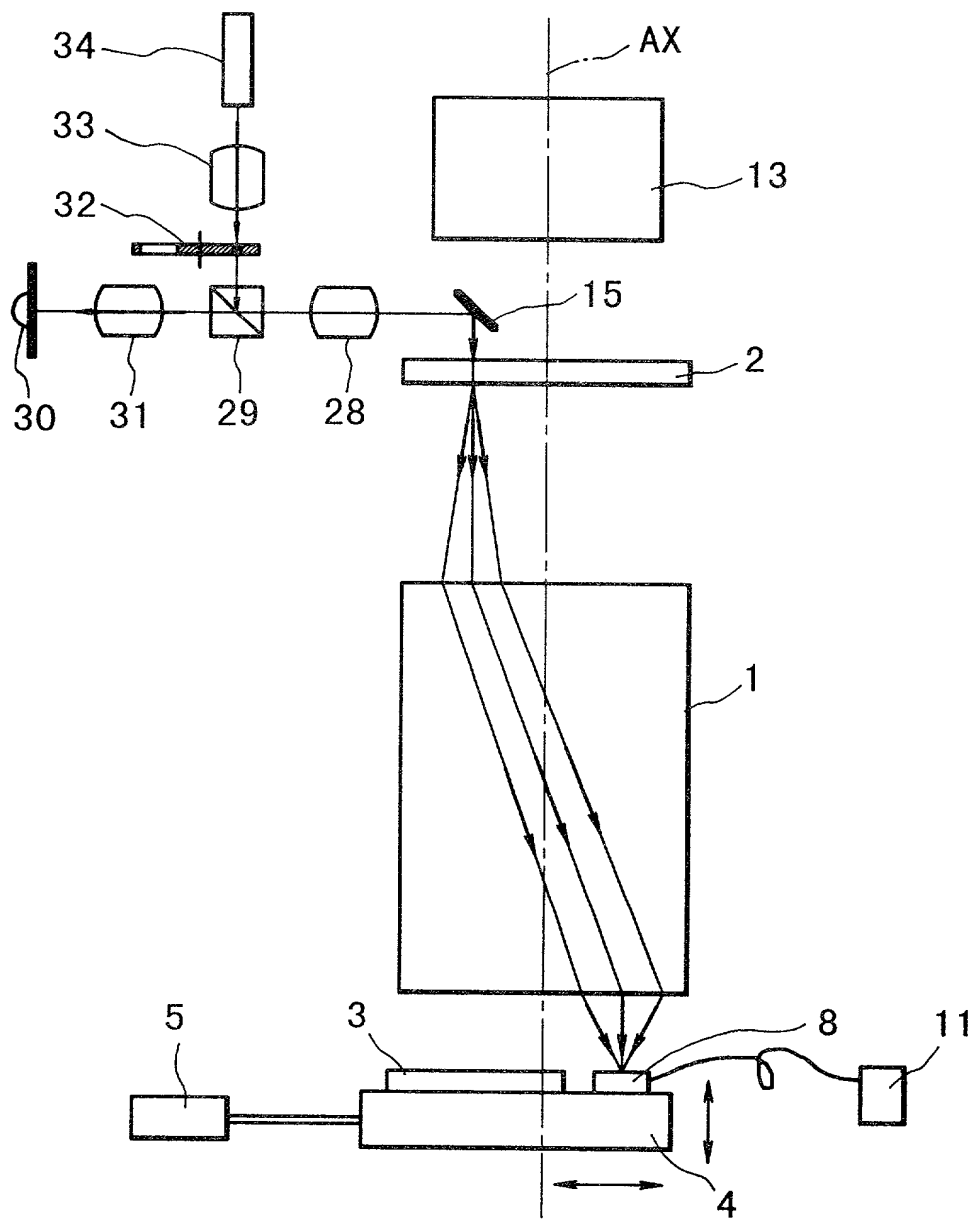


FIG. 7



**FIG. 8**

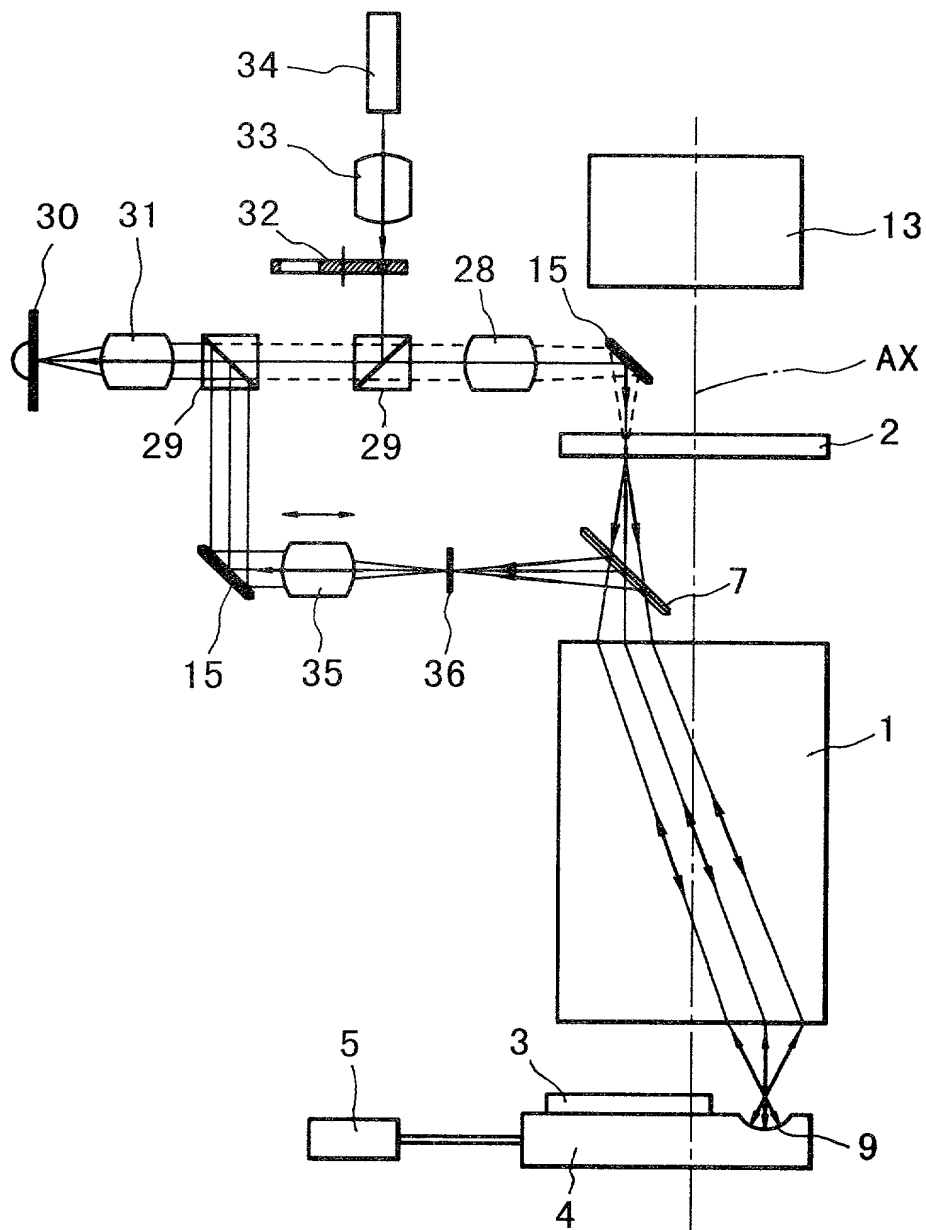


FIG. 9

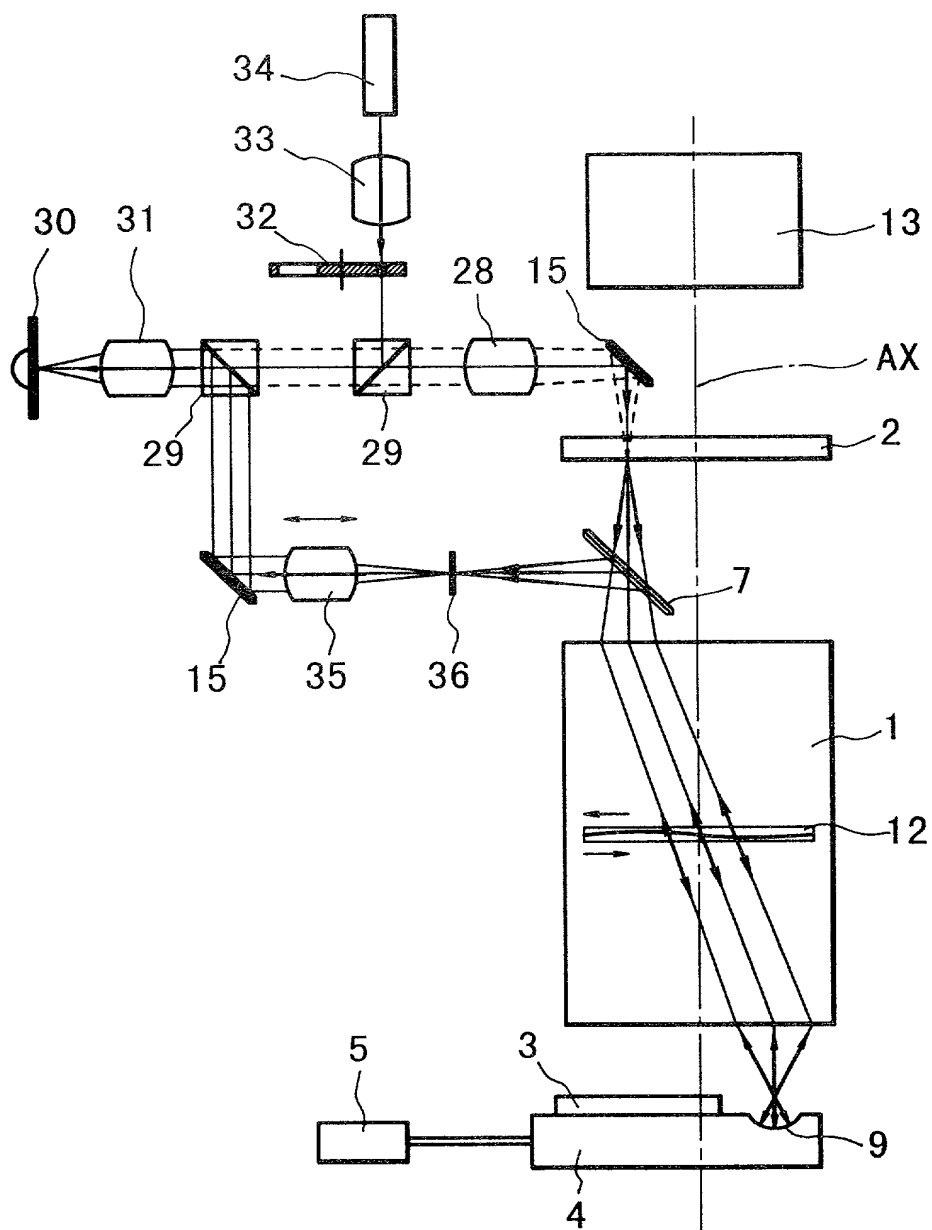
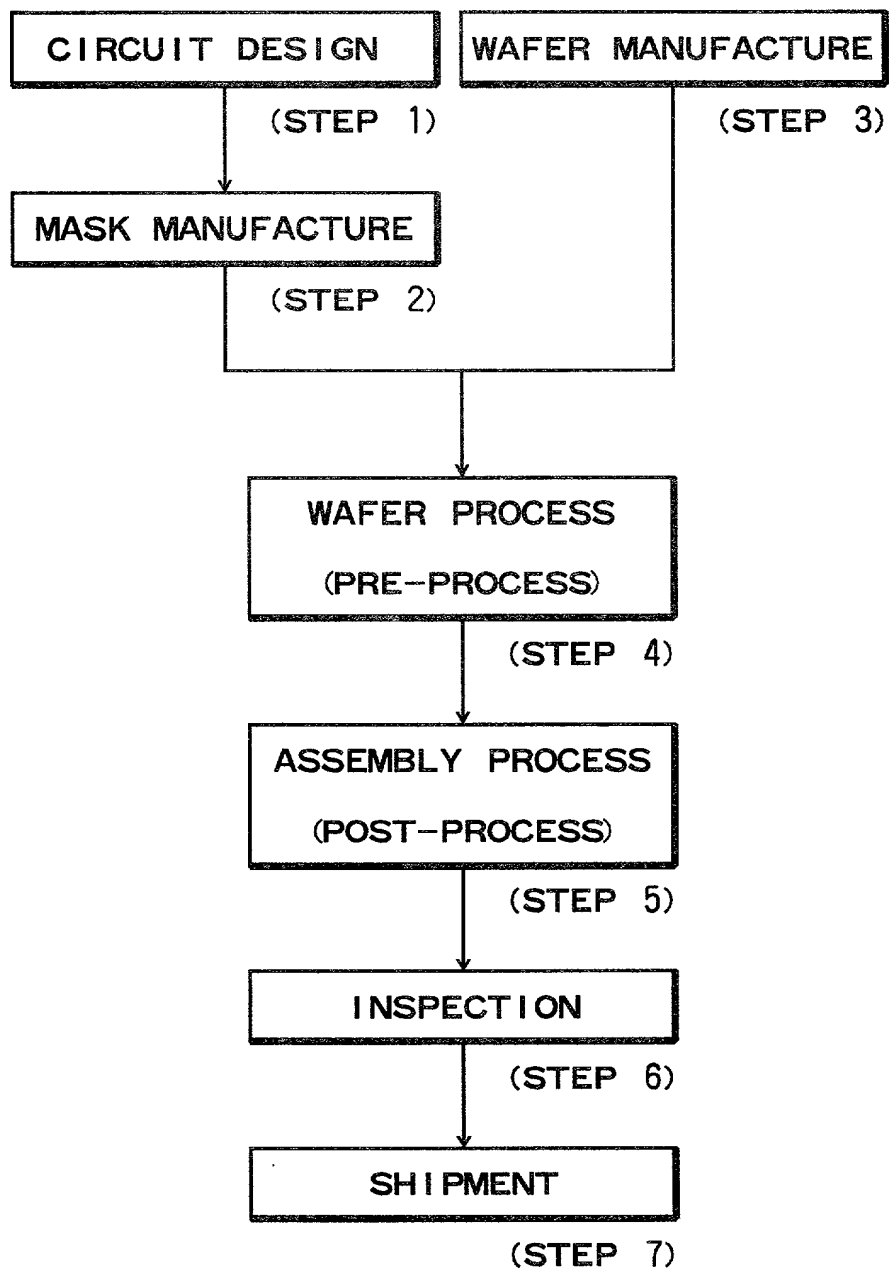


FIG. 10



**FIG. II**

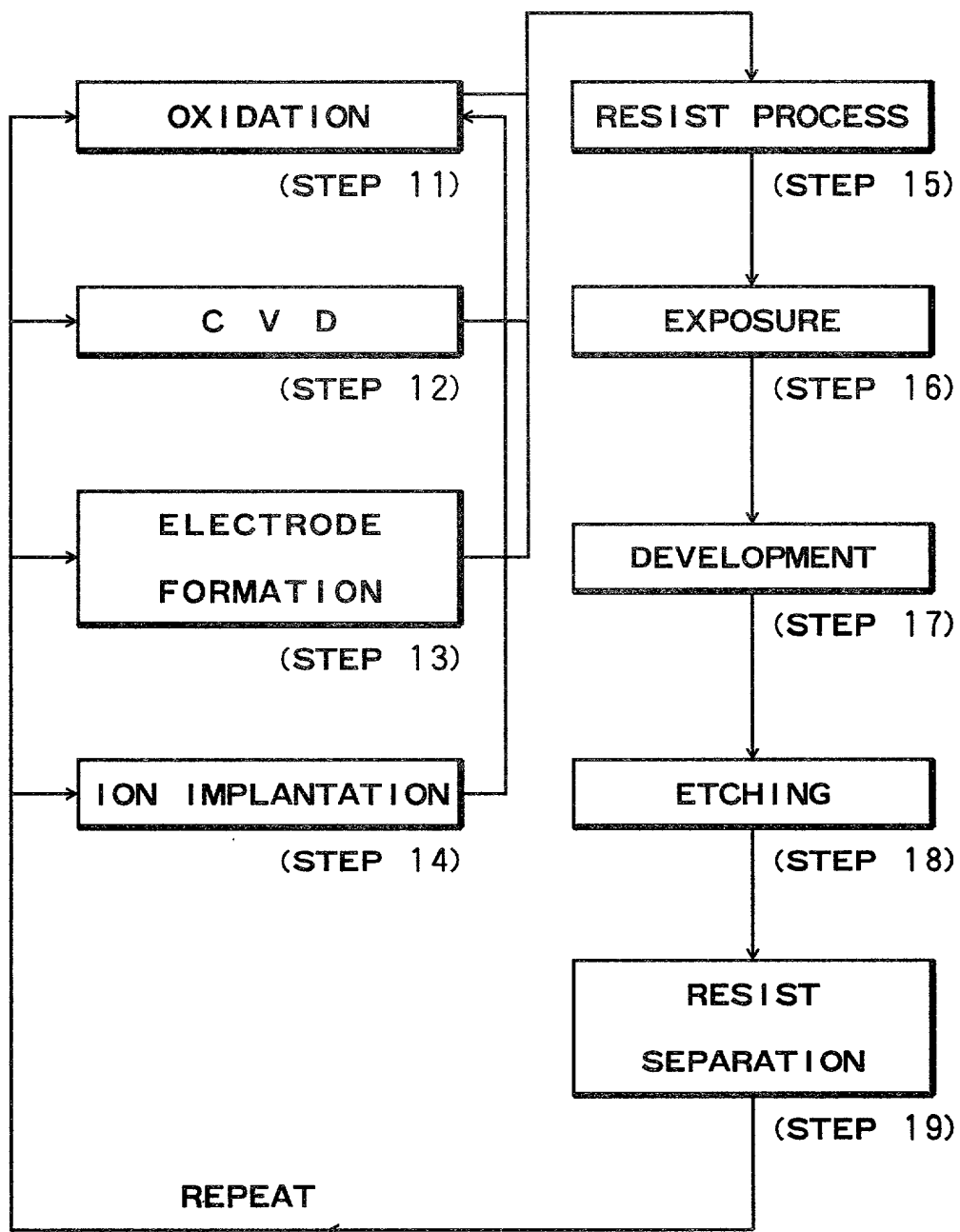


FIG. 12

COMBINED DECLARATION AND POWER OF ATTORNEY  
FOR PATENT APPLICATION

(Page 1)

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled PROJECTION EXPOSURE APPARATUS, AND DEVICE MANUFACTURING METHOD USING THE SAME

the specification of which ☒ is attached hereto ☐ was filed on \_\_\_\_\_ as United States Application No. or PCT International Application No. \_\_\_\_\_ and was amended on \_\_\_\_\_ (if applicable).

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR §1.56.

I hereby claim foreign priority benefits under 35 U.S.C. §119(a)-(d) or §365(b), of any foreign application(s) for patent or inventor's certificate, or § 365(a) of any PCT international application which designates at least one country other than the United States, listed below and have also identified below any foreign application for patent or inventor's certificate, or PCT international application having a filing date before that of the application on which priority is claimed:

Country	Application No.	Filed (Day/Mo./Yr.)	(Yes/No) Priority Claimed
JAPAN	11-157039	03 June 1999	YES

I hereby claim the benefit under 35 U.S.C. § 120 of any United States application(s), or § 365(c) of any PCT international application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT international application in the manner provided by the first paragraph of 35 U.S.C. § 112, I acknowledge the duty to disclose information which is material to patentability as defined in 37 C.F.R. § 1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application.

Application No.	Filed (Day/Mo./Yr.)	Status (Patented, Pending, Abandoned)
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I hereby appoint the practitioners associated with the firm and Customer Number provided below to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith, and direct that all correspondence be addressed to the address associated with that Customer Number:

**FITZPATRICK, CELLA, HARPER & SCINTO**  
Customer Number: 05514

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon

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COMBINED DECLARATION AND POWER OF ATTORNEY  
FOR PATENT APPLICATION  
(Page 2)

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